

SOME DEGENERATE TRANSONIC FLOWS

(NEKOTORYE VYROZHDENNIYE OKOLOZVUKOVYYE TECHENIIA)

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O. S. RYZOV
(Moscow)

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We consider transonic motions of an ideal gas which are represented in the velocity hodograph by a curve or by a surface. In the second part of the note we determine a class of self-similar solutions representing plane and axially symmetric flows.

1. Three-dimensional flows with a degenerate hodograph. 1. The equations of a transonic three-dimensional gas flow in cartesian coordinates read

$$\begin{aligned} uu_x - v_y - w_z = 0, \quad u_y - v_x = 0, \quad u_z - w_x = 0, \quad v_z - w_y = 0 \\ u = (\kappa + 1) \frac{U}{a_*}, \quad v = (\kappa + 1) \frac{V}{a_*}, \quad w = (\kappa + 1) \frac{W}{a_*} \end{aligned} \quad (1.1)$$

Here κ is the adiabatic exponent, U, V, W the perturbation velocity components along the x, y, z axes, the undisturbed velocity vector having the magnitude of the critical speed a_* and being directed along the x axis.

Let us consider double waves, that is flows for which only the two quantities v and w are independent, and

$$u = u(v, w) \quad (1.2)$$

Using (1.2) and equations (1.1) we obtain

$$(uu_v^2 - 1)v_y + 2uu_v u_w v_z + (uu_w^2 - 1)w_z = 0 \quad (1.3)$$

Every plane $x = \text{const.}$ of the physical space is mapped in the velocity hodograph space onto the same surface Σ . Hence we may consider in equations (1.3) the variables v and w as independent, and the variables y and z as functions of these independent variables. We have

$$r_y = z_w \Delta, \quad r_z = -y_w \Delta, \quad w_z = y_v \Delta, \quad \Delta = v_y w_z - v_z^2$$

and by equation (1.3)

$$(uu_v^2 - 1)z_w - 2uu_v u_w y_w + (uu_w^2 - 1)y_v = 0 \quad (1.4)$$

Consider now the function χ determined by the equation [1]

$$\chi = ux + vy + wz - \varphi \quad (u = \varphi_x, v = \varphi_y, w = \varphi_z) \quad (1.5)$$

Its differential is $d\chi = (y + xu_v)dv + (z + xu_w)dw$. Hence

$$\chi_v = y + xu_v, \quad \chi_w = z + xu_w \quad (1.6)$$

Differentiating equations (1.6) for $x = \text{const.}$ we obtain

$$y_v = \chi_{vv} - xu_{vv}, \quad y_w = \chi_{vw} - xu_{vw}, \quad z_w = \chi_{ww} - xu_{ww} \quad (1.7)$$

Now we substitute relations (1.7) into equation (1.4). Setting the term not containing z and the term containing z in the first degree equal to zero, we obtain two equations which determine the functions w and χ :

$$\begin{aligned} (uu_w^2 - 1)u_{vv} - 2uu_vu_wu_{vw} + (uu_v^2 - 1)u_{ww} &= 0 \\ (uu_w^2 - 1)\chi_{vv} - 2uu_vu_w\chi_{vw} + (uu_v^2 - 1)\chi_{ww} &= 0 \end{aligned} \quad (1.8)$$

After equations (1.8) are solved, formulas (1.6) [1] give the transformation to the physical space. In the case of conical flows we have $\chi = 0$ and $y/x = -u_v$, $z/x = -u_w$.

2. We note one particular solution of the first equation (1.8).

One easily sees that this equation admits the transformation group $U(v, w) = a_1^{-2/3}u(a_1v, a_1w)$, where a_1 is an arbitrary non-vanishing constant. Therefore equations (1.8) have a solution of the form

$$u = v^{3/2}f_1(\xi_1), \quad \xi_1 = w/v \quad (1.9)$$

where the function f_1 satisfies the ordinary differential equation

$$\left(\xi_1^2 - 2\xi_1^2 f_1 f_1' + \frac{4}{9} f_1^3\right) f_1'' + \frac{2}{9} f_1^2 f_1'^2 - \frac{2}{3} \xi_1 f_1' + \frac{2}{9} f_1 = 0 \quad (1.10)$$

This equation is itself invariant under the transformation group $\Phi_1(\xi_1) = a_2^{-2/3}f(a_2\xi_1)$, therefore its order may be lowered. Indeed, setting $f_1 = \xi_1^{3/2}F_1(\eta_1)$, $\eta_1 = \ln|\xi_1|$, we transform equation (1.10) into an equation which does not contain the independent variable explicitly. Next, setting $dF_1/d\eta_1 = \Psi_1$ and taking F_1 as the independent variable, we obtain the first order equation

$$\frac{d\Psi_1}{dF_1} = \frac{4/9 F_1 + 1/9 \Psi_1 + 2/9 F_1 \Psi_1^3 + 2/9 F_1^2 \Psi_1^2 - 4/9 F_1^3 \Psi_1 - 16/81 F_1^4}{\Psi_1(1 - 4/9 F_1^3 - 8/9 F_1^2 \Psi_1 - 2 F_1 \Psi_1^2)} \quad (1.11)$$

Solving equation (1.11) and carrying out the second integration

$$\eta_1 - \eta_0 = \int \frac{dF_1}{\Psi_1(F_1)}$$

where η_0 is an arbitrary constant, we go over to the physical space by the formulas

$$\frac{y}{x} = \frac{w^{3/2}}{v} \frac{dF_1}{d\eta_1}, \quad \frac{z}{x} = \frac{1}{w^{1/2}} \left(\frac{2}{3} F_1 + \frac{dF_1}{d\eta_1} \right) \quad (1.12)$$

3. Let us consider axially symmetric flows of the class discussed above. We have that

$$u = u(\omega), \quad \omega = \sqrt{v^2 + w^2} \quad (1.13)$$

and the first equation (1.8) implies that

$$\omega u'' - uu'^3 + u' = 0 \quad (1.14)$$

Interchanging dependent and independent we obtain the well known equation solved by Busemann [2]:

$$\omega \omega'' = \omega'^2 - u \quad (1.15)$$

4. The differential equation of the characteristics of the first equation (1.8) reads

$$(uu_w^2 - 1)dw^2 + 2uu_v u_w dv dw + (uu_v^2 - 1)dv^2 = 0 \quad (1.16)$$

Noting that along the surface Σ we have $du = u_v dv + u_w dw$, we obtain from (1.16) the equation

$$u du^2 = dv^2 + dw^2 \quad (1.17)$$

This equation determines characteristic curves S_+ and S_- on the surface Σ . One can show that simple waves are described by such an equation. In this case the whole flow is mapped onto a single S curve in the velocity hodograph.

The formulas

$$u = \left(\frac{3}{2}\tau\right)^{2/3}, \quad v = \int \cos f_2(\tau) d\tau, \quad w = \int \sin f_2(\tau) d\tau \quad (1.18)$$

solve equation (1.17). The corresponding flow in the physical space is given by the relation

$$\left(\frac{3}{2}\tau\right)^{-1/3}x + \cos f_2(\tau)y + \sin f_2(\tau)z + F_2(\tau) = 0 \quad (1.19)$$

where $f_2(r)$ and $F_2(r)$ are arbitrary functions of r . This solution can be used in computing certain aerofoils.

2. Self-similar plane and axially symmetric flows. 1. We consider now plane and axially symmetric flows. In this case we have by (1.1)

$$-uu_x + \omega_r + \delta\omega/r = 0, \quad u_r = \omega_x \quad (2.1)$$

Here ω is the component of the perturbation velocity (1) in the direction of the radius r , $\delta = 0$ for plane flows and $\delta = 1$ for axially symmetric flows.

The system of equations (2.1) is invariant under the continuous transformation group

$$U(x, r) = \alpha_3^{2(1-\beta)}u(\alpha_3^\beta x, \alpha_3 r), \quad \Omega(x, r) = \alpha_3^{3(1-\beta)}\omega(\alpha_3^\beta x, \alpha_3 r) \quad (2.2)$$

where α_3 and β are arbitrary constants. Hence system (2.1) must possess self-similar solutions of the form [3, 7]

$$u = x^{2(\beta+1)}f_3(\xi_2), \quad \omega = x^{3(\beta+1)}f_4(\xi_2), \quad \xi_2 = rx^\beta \quad (2.3)$$

In fact, substituting the expressions (2.3) into the equations (2.1) we obtain

$$f_3' = 3(\beta + 1)f_4 + \beta \xi_2 f_4', \quad -2(\beta + 1)f_3^2 - \beta \xi_2 f_3 f_3' + f_4' + \delta f_4 / \xi_2 = 0 \quad (2.4)$$

Eliminating the function f_4 from the system (2.4) we obtain a single second order equation for the function f_3 :

$$(\beta^2 \xi_2^2 f_3 - 1) f_3'' + (9\beta + 7) \beta \xi_2 f_3 f_3' + \beta^2 \xi_2^2 f_3'^2 + 2(4\beta^2 + 7\beta + 3) f_3^2 - \delta f_3' / \xi_2 = 0 \quad (2.5)$$

It is easy to see that equation (2.5) is itself invariant under the transformation group $\Phi_3(\xi_2) = \alpha_4^2 f_3(\alpha_4 \xi_2)$, where α_4 is an arbitrary constant. Setting $f_3 = \xi_2^{-2} F_3(\eta_2)$, $\eta_2 = \ln |\xi_2|$ we transform equation (2.5) into an equation which does not contain the independent variable explicitly. Next, setting $f_3 = \xi_2^{-2} F_3(\eta_2)$, $\eta_2 = \ln |\xi_2|$, and taking F_2 as the independent variable we obtain the first order equation

$$\frac{d\Psi_3}{dF_3} = \frac{(\delta - 5) \Psi_3 + 2(3 - \delta) F_3 - \beta^2 \Psi_3^2 - 7\beta \Psi_3 F_3 - 6F_3^2}{\Psi_3(\beta^2 F_3 - 1)} \quad (2.6)$$

The functions f_4 and F_3 are connected by the relation

$$f_4 = \frac{\xi_2^{-3}}{3\beta + 3 - \delta\beta} (F_3' - 2F_3 - 2\beta F_3^2 - \beta^2 F_3 F_3') = \xi_2^{-3} R(\eta_2) \quad (2.7)$$

The perturbation velocity components are given by

$$u = \left(\frac{x}{r}\right)^2 F_3(\eta_2), \quad \omega = \left(\frac{x}{r}\right)^3 R(\eta_2) \quad (2.8)$$

2. Consider the case $\beta = 0$. Then $u = x^2 f_3(r)$, $\omega = x^3 f_4(r)$, so that the variables x and r are separated and we obtain solutions studied by Zigulev [4] $f_3 = \zeta_2^{-2(\beta+1)} f_5(\zeta_2)$, $f_4 = \zeta_2^{-3(\beta+1)} f_6(\zeta_2)$, $\zeta_2 = \xi_2^{1/\beta}$, $1/\beta = \gamma$ (2.9)

Using (2.4) we obtain for the functions $f_5(\zeta_2)$ and $f_6(\zeta_2)$ the system of equations

$$-2(\gamma + 1) f_5 + \gamma \zeta_2 f_5' = f_6', \quad -f_5 f_5' + (\delta - 3 - 3\gamma) f_6 + \gamma \zeta_2 f_6' = 0 \quad (2.10)$$

Consider, in particular, the case $\gamma = 0$. Then $u = r^{-2} f_5(x)$, $\omega = r^{-3} f_6(x)$, that is, the variables x and r are separated and we obtain another type of flows studied in the paper just quoted.

3. Consider now the case $\beta = -\frac{1}{2}$. It is easy to verify that in this case equation (2.6) admits the solution

$$\Psi_3 = 2(1 + \delta) \left(1 + \frac{2}{1 + \delta} F_3 \pm \sqrt{1 + \frac{2}{1 + \delta} F_3} \right) \quad (2.11)$$

Using (2.11) one easily obtains the relation

$$f_3 = A + \frac{A^2}{2(1 + \delta)} \xi_2^2 \quad (2.12)$$

The perturbation velocity components are now given by

$$u = Ax + \frac{A^2}{2(1 + \delta)} r^2, \quad \omega = \frac{A^2}{1 + \delta} xr + \frac{A^3}{2(1 + \delta)(3 + \delta)} r^3 \quad (2.13)$$

If the gas flow considered is two-dimensional, so that $\delta = 0$, then the relations (2.13) are the solution due to Falkovich [5] which describe

the shockless flow in a nozzle near the sonic line. If $\delta = 1$, the equations (2.13) describe an axially symmetric flow in an axially symmetric nozzle. The equation of the sonic line reads

$$x = -\frac{A}{2(1+\delta)} r^2 \quad (2.14)$$

This equation shows that in an axially symmetric nozzle the sonic line is closer to a vertical straight line than it would be in a plane nozzle for the same value of the constant A . This constant equals the derivative u_x at the center of the nozzle.

3. Plane and axially symmetric flows limiting to self-similar ones.

1. We consider first plane transonic flows. In this case $\delta = 0$ and equations (2.1) are invariant under the transformations $r = r_0 + r'$. We use the method of the paper [6] in which it was shown how to obtain, by a limiting process, a new class of solutions from a class of self-similar solutions containing an arbitrary exponent which may be increased indefinitely. The solutions given in 2(2) have this property. After some calculations we obtain

$$u = e^{-2mr} f_7(\xi_3), \quad \omega = e^{-3mr} f_8(\xi_3), \quad \xi_3 = xe^{mr} \quad (3.1)$$

where the functions f_7 and f_8 satisfy the system of ordinary differential equations

$$-f_7 f_7' - 3m f_8 + m \xi_3 f_8' = 0, \quad -2m f_7 + m \xi_3 f_7' = f_8' \quad (3.2)$$

(a limiting form of the equations in 2(2)).

Eliminating from (3.2) the function f_8 we obtain a single second order differential equation for the function f_7 :

$$(m^2 \xi_3^2 - f_7) f_7'' - f_7'^2 - 3m' \xi_3 f_7' + 4m^2 f_7 = 0 \quad (3.3)$$

This equation is invariant under the group $\Phi_4(\xi_3) = \alpha_5^{-2} f_7(\alpha_5 \xi_3)$ and can be reduced to a first order equation

$$\frac{d\Psi_4}{dF_4} = \frac{6F_4^2 + 7F_4\Psi_4 + \Psi_4^2}{\Psi_4(m^2 - F_4)} \quad (3.4)$$

Here

$$\eta_3 = \ln |\xi_3|, \quad f_7 = \xi_3^2 F_4(\eta_3), \quad \Psi_4 = \frac{dF_4}{d\eta_3} \quad (3.5)$$

The perturbation velocity components are given by

$$u = x^2 F_4 \quad (3.6)$$

$$\omega = \frac{x^3}{3m} (m^2 F_4' - F_4 F_4' - 2F_4^2)$$

If $m = 0$, then the functions f_7 and f_8 are constant and we have a uniform flow. For $m \neq 0$ the integral curves of equation (3.4) are shown on Fig. 1. The essential characteristic of the flows just considered is their

asymmetry with respect to the axis $r = 0$.

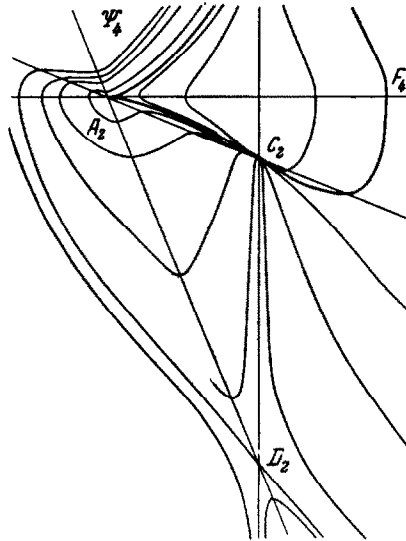


Fig. 1.

2. We consider now plane and axially symmetric flows simultaneously. Using the invariance of equations (2.1) with respect to the transformations $x = x_0 + x'$ we obtain from relations (2.3) a new class of solutions. These solutions, obtained by letting the exponent β increase indefinitely, have the form [6]

$$u = e^{2nx} f_9 (\xi_4), \quad \omega = e^{3nx} f_{10} (\xi_4), \quad \xi_4 = re^{nx} \tag{3.7}$$

where the functions f_9 and f_{10} are determined by the equations

$$-2nf_9^3 - n\xi_4 f_9 f_9' + f_{10}' + \delta f_{10} / \xi_4 = 0, \quad f_9' = 3nf_{10} + n\xi_4 f_{10}' \tag{3.8}$$

(limiting case of equations (2.3)). The function f_9 must satisfy the equation

$$(n^2 \xi_4^2 f_9 - 1) f_9'' + 9n^2 \xi_4 f_9 f_9' + n^2 \xi_4^2 f_9'^2 + 8n^2 f_9^2 - \delta f_9' / \xi_4 = 0 \tag{3.9}$$

As before we introduce new variables

$$\eta_4 = \ln \xi_4, \quad f_9 = \xi_4^{-2} F_5 (\eta_4), \quad \Psi_5 = \frac{dF_5}{d\eta_4} \tag{3.10}$$

and obtain a single first order equation

$$\frac{d\Psi_5}{dF_5} = \frac{(\delta - 5) \Psi_5 + 2(3 - \delta) F_5 - n^2 \Psi_5^2}{\Psi_5 (n^2 F_5 - 1)}$$

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